

A Fictitious Domain Method for FSI Simulations

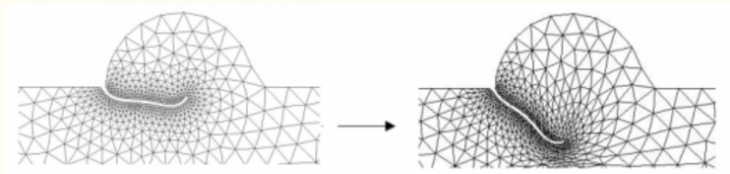
Maria Nestola, Patrick Zulian, Rolf Krause

Postdoctoral Research Associate,
Institute of Computational Science
Università della Svizzera italiana

SCCER-SOE Conference,
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- **Several approaches** have been developed to reproduce the **interaction between a fluid and a solid structure**:

Boundary-fitted method

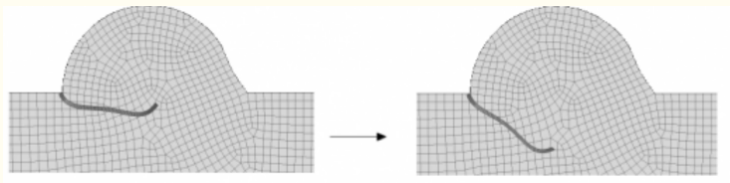


Guarantees accurate results at the interface between the solid structure and the fluid flow.

Scenarios with **large displacements** → **distorted fluid grid** may affect the numerical stability of the problem and the accuracy of the solution.

- **Several approaches** have been developed to reproduce the **interaction** between a **fluid** and a **solid structure**:

Embedded Boundary method



Designed to embed the solid phase within the fluid phase, enabling the calculation of the FSI effect on a stationary fluid grid which can be analysed in a purely Eulerian fashion.

Solving the FSI problem implies the necessity to couple a fluid and a structure problem.

Requirement

1. **transfer of data** between **different non matching meshes**
non conforming approximation spaces
2. numerical simulations of **complex** and **large scale** problems
3. use of supercomputers: **meshes arbitrarily distributed among processors**

The way the transfer operators are constructed affects **convergence**, **accuracy** and **efficiency**

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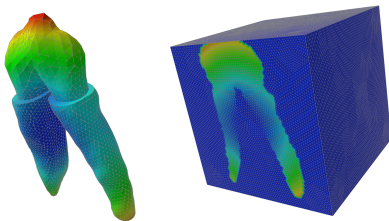
L^2 -**projection MOONoLith**: library developed at ICS
(<http://moonolith.inf.usi.ch>)

Krause, Rolf, and Patrick Zulian. "A Parallel Approach to the Variational Transfer of Discrete Fields between Arbitrarily Distributed Unstructured Finite Element Meshes." SIAM Journal on Scientific Computing 38.3 (2016): C307-C333.)

MOONoLith

(<http://moonolith.inf.usi.ch>)

Transfer the data from a **source** space to a **target** space



Source and Target Mesh

$\Omega_v, \Omega_w \subset \mathbb{R}^d \rightarrow$ bounded domains approximated by Ω_v^h and Ω_w^h ,

\mathcal{T}_v^h and $\mathcal{T}_w^h \rightarrow$ associated meshes,

$V_h = V_h(\mathcal{T}_v^h)$ and $W_h = W_h(\mathcal{T}_w^h) \rightarrow$ associated spaces.

For the definition of the projection operator, one needs to define a **suitable discrete space of Lagrange multipliers** M_h .

Set M_h as a **discrete space based on the same space as the target space**.

$$\int_{I_h} (v_h - P(v_h)) \mu_h \, d\mathbf{x} = \int_{I_h} (v_h - w_h) \mu_h \, d\mathbf{x} = 0 \quad \forall \mu_h \in M_h. \quad (1)$$

\Downarrow

$$\sum_{i \in J_v} v_i \int_{I_h} \phi_i \psi_k \, d\mathbf{x} = \sum_{j \in J_w} w_j \int_{I_h} \theta_j \psi_k \, d\mathbf{x} \quad \text{for } k \in J_\mu. \quad (2)$$

\Downarrow

$$\mathbf{w} = \mathbf{D}^{-1} \mathbf{B} \mathbf{v} = \mathbf{T} \mathbf{v}.$$

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⇓

$$\sum_{i \in J_v} v_i \int_{I_h} \phi_i \psi_k \, d\mathbf{x} = \sum_{j \in J_w} w_j \int_{I_h} \theta_j \psi_k \, d\mathbf{x} \quad \text{for } k \in J_\mu. \quad (4)$$

⇓

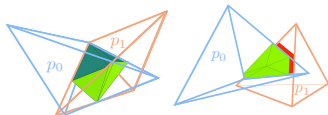
pseudo L^2 projection

$$(\psi_k, \theta_j)_{L^2(I_h)} = \delta_{j,k} (\theta_j, \mathbf{1})_{L^2(I_h)} \quad \forall j, k \in J_w. \quad (5)$$

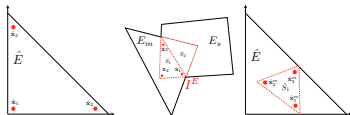
⇓

D \Rightarrow diagonal matrix

1. Transfer data, \mathbf{v} , from E_m to data, \mathbf{w} , on E_s requires finding mesh intersections for quadrature.



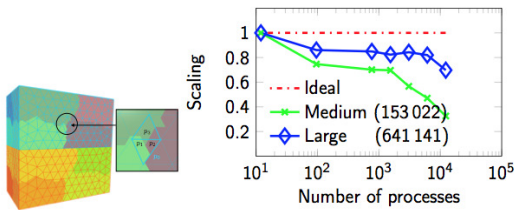
2. Intersection-Detection: parallel tree-search algorithm. Outcome: element pairs (associated with processes).
3. Generate the quadrature points for integrating in the intersection region I^E .



4. Compute the local element-wise contributions for the operators \mathbf{B} and \mathbf{D} . Assemble one matrix \mathbf{T} containing all the different projection matrices $\mathbf{T}_{m,s}$ for every pair of intersecting meshes:

$$\mathbf{T} = \begin{bmatrix} \mathbf{T}_{1,1} & \mathbf{T}_{1,2} & \cdots & \mathbf{T}_{1,n} \\ \vdots & & \ddots & \vdots \\ \mathbf{T}_{n,1} & \mathbf{T}_{n,2} & \cdots & \mathbf{T}_{n,n} \end{bmatrix}$$

Weak Scaling Tests



Find $(\mathbf{u}_f, p_f; \boldsymbol{\eta}_s, p_s; \boldsymbol{\lambda}) \in (V_f \times Q_f \times V_s \times Q_s \times L)$ such that for every $(\mathbf{v}_f, q_f; \mathbf{v}_s, q_s; \boldsymbol{\mu}) \in (V_f \times Q_f \times V_s \times Q_s \times L)$

$$\int_{\Omega_f} \rho_f \frac{\partial \mathbf{u}_f}{\partial t} \cdot \mathbf{v}_f dV + \int_{\Omega_f} \rho_f [(\mathbf{u}_f \cdot \nabla) \mathbf{u}_f] \cdot \mathbf{v}_f dV + \int_{\Omega_f} \boldsymbol{\sigma}(\mathbf{u}_f, p_f) : \nabla \mathbf{v}_f dV - \int_{\mathcal{I}} \boldsymbol{\lambda} \cdot \mathbf{u}_f dV = 0$$

$$\int_{\Omega_f} q_f \nabla \cdot \mathbf{u}_f dV = 0$$

$$\int_{\mathcal{I}} \boldsymbol{\mu} \cdot \left(\frac{\partial \boldsymbol{\eta}_s}{\partial t} - \mathbf{u}_f \right) dV = 0$$

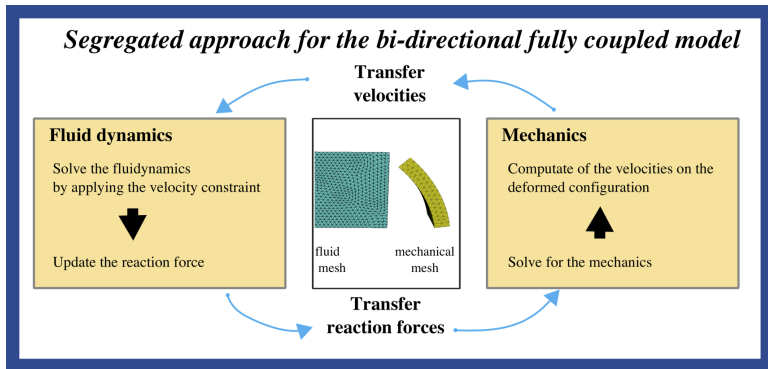
$$\int_{\widehat{\Omega}_s} \widehat{\rho}_s \frac{\partial^2 \widehat{\boldsymbol{\eta}}_s}{\partial t^2} \cdot \widehat{\mathbf{v}}_s + \int_{\widehat{\Omega}_s} \widehat{\mathbf{P}}(\widehat{\mathbf{F}}) : \nabla \widehat{\mathbf{v}}_s dV + \int_{\mathcal{I}} \boldsymbol{\lambda} \cdot \mathbf{v}_s dV = 0$$

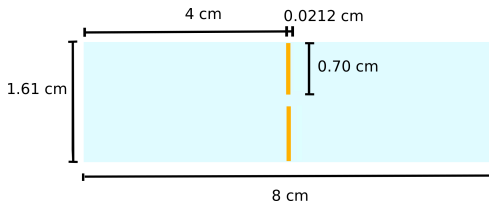
$\widehat{\Omega}_s$: solid domain, Ω_f : fluid domain $\mathcal{I} := \widehat{\Omega}_s \cap \Omega_f$.

"A fictitious domain/mortar element method for fluid-structure interaction." International Journal for Numerical Methods in Fluids 35.7 (2001): 743-761.

Segregated Approach

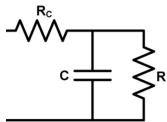
- 1 decoupled variables
- 2 iterations between subproblems
- 3 fixed point iteration





Boundary Conditions

- 1 Inlet: Parabolic Profile $v_{fluid}(t) = 5y(y - 1.61)[\sin(2\pi t) + 1.1]$
- 2 Outlet: Windkessel Model

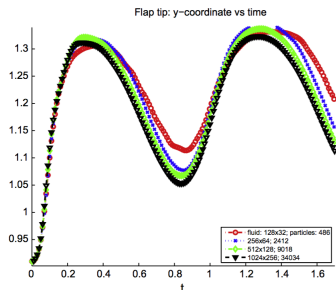
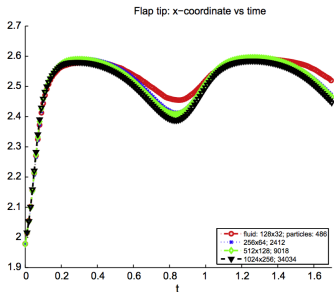
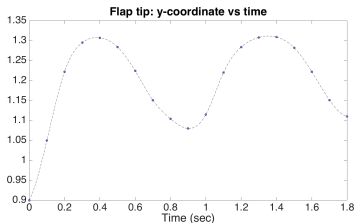
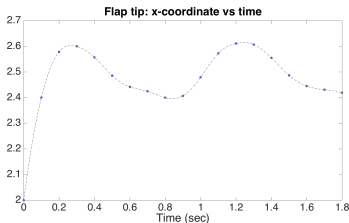


$$Q(t) = C \frac{dP(t)}{dt} + \frac{P(t)}{R} \quad P_{outlet}(t) = Q(t) \cdot R_c + P(t)$$

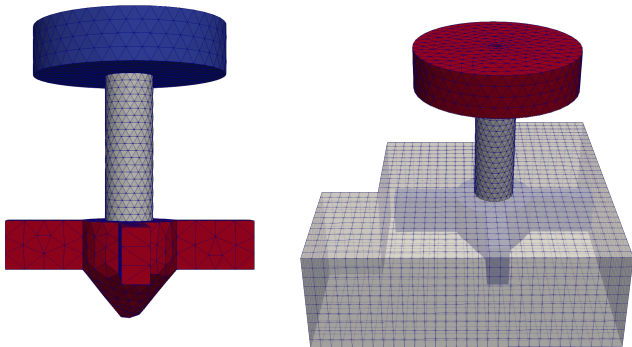
- 3 No slip boundary conditions on the top and on the bottom

Gil, Antonio J., et al. J. Computational Physics 229 (2010): 8613-8641.

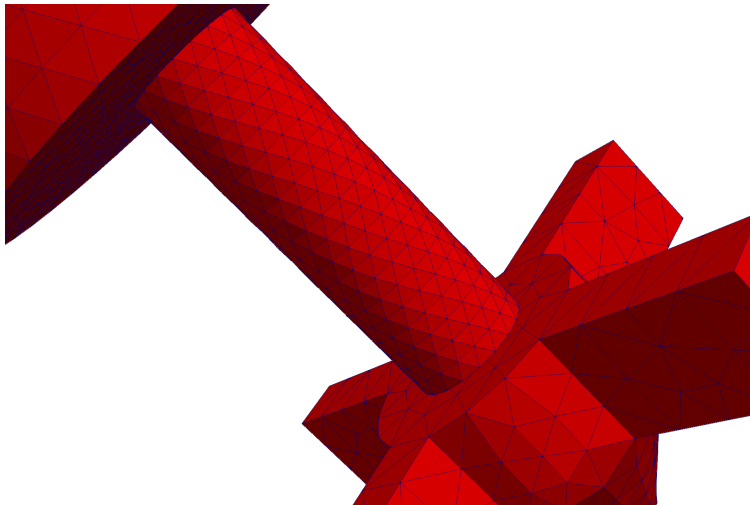
- 1 Neo-Hookean constitutive model: Beams with different stiffness
- 2 Newtonian fluid

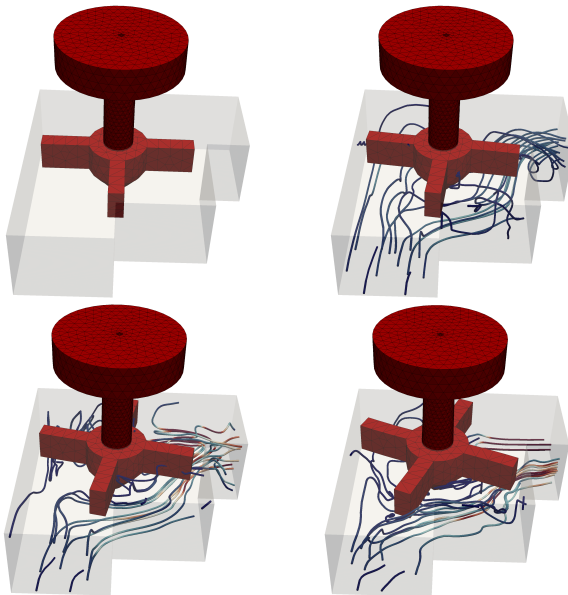


- 1 Linear constitutive model for the turbine blades
- 2 Newtonian fluid, Reynolds Number=2000
- 3 Non Conforming Meshes (Fluid and Solid Grid)



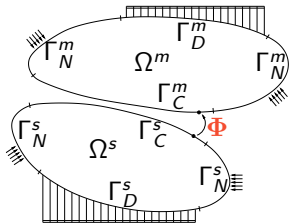
1 Non Conforming Meshes





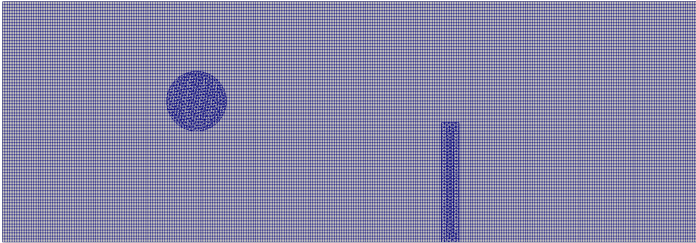
- $\Omega = \Omega^m \cup \Omega^s \subset \mathbb{R}^3$ two bodies
 $\Gamma_D = \Gamma_D^m \cup \Gamma_D^s$ Dirichlet boundary
 $\Gamma_N = \Gamma_N^m \cup \Gamma_N^s$ Neumann boundary
 $\Gamma_C = \Gamma_C^m \cup \Gamma_C^s$ possible contact boundary
- Find displacement $\mathbf{u} = (\mathbf{u}^m, \mathbf{u}^s)$ s. t.

$$\begin{aligned} -\sigma_{ij}(\mathbf{u})_{,j} &= f_i && \text{in } \Omega, \\ \mathbf{u} &= \mathbf{0} && \text{on } \Gamma_D, \\ \sigma_{ij}(\mathbf{u})n_j &= \bar{t}_i && \text{on } \Gamma_N. \end{aligned}$$



- $\Phi : \Gamma_C^s \rightarrow \Gamma_C^m$: bijective “contact mapping”, \mathbf{n}^Φ : induced normal field, d : initial gap
 $[u] := (\mathbf{u}^s - \mathbf{u}^m \circ \Phi) \cdot \mathbf{n}^\Phi$: jump in \mathbf{n}^Φ -direction
- Enforce contact conditions on Γ_C :

$$\begin{aligned} \sigma_t(\mathbf{u}^m) &= \sigma_t(\mathbf{u}^s) = \mathbf{0} && \text{no friction} \\ \sigma_n(\mathbf{u}^m \circ \Phi) &= \sigma_n(\mathbf{u}^s) \leq 0 && \text{force balance} \\ ([u] - d)\sigma_n(\mathbf{u}^s) &= 0 && \text{complementarity condition} \\ [u] &\leq d && \text{no penetration (linearized)} \end{aligned}$$



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Solve contact problem

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Efficient and flexible way to treat the coupling on the volume on the interface by means of the L^2 – *projection* approach

The use of the L^2 – *projection* approach (MOONoLith library) allows for coupling arbitrary "in-house" solver codes based on different kind of spaces discretizations (Finite Element, Finite Volume, Finite differences), (i.e AV-Flow, (Artrog Center, Bern))

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Future Applications: flow in fractured networks, friction between rocks

Thank you for your attention